



An Introduction to Plumbing and Gas Systems for Medical Facilities

By

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An Introduction to Plumbing and Gas Systems for Medical Facilities



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1. GENERAL.

This discussion provides an introduction to plumbing and medical gas systems for medical, dental, training, and research facilities (hereinafter, Medical Treatment Facility). The primary purpose of these systems is to provide safe and reliable support to the medical mission. In addition, appropriate design consideration shall be given to ensure system maintainability, economy and energy efficiency, and adaptability to future facility modification or expansion.. This information is an introduction only to this topic. Designers must always be guided in project design by current and applicable codes, standards and practices.

1.1 PLUMBING SYSTEMS. Plumbing systems include domestic cold and hot water; sanitary, storm, and industrial (acid) waste drainage; water treatment (such as softening, deionization, reverse osmosis); fuel gas; and landscape irrigation. Plumbing systems shall be designed to be safe reliable and maintainable. Selection of materials, equipment, and installation techniques shall consider life cycle cost effectiveness and maintainability in addition to medical functional requirements. Potable water distribution pipe 50 mm (2") and smaller shall be copper. Designers are specifically alerted to provide for appropriate system isolation and balancability, and necessary equipment and design practices to avoid cross connections and backflow.

1.2 WATERBORNE PATHOGEN PREVENTION/CONTROL. The Center for Disease Control (CDC), the American Society of Heating, Refrigeration, and Air-Conditioning Engineers (ASHRAE), the American Society for Healthcare Engineering (ASHE) and the Joint Commission on Accreditation of Healthcare Organizations (JCAHO) have cited two main means by which waterborne pathogens are introduced into medical treatment facilities - by the water supply system and cooling towers. Water-borne bacteria, chiefly Legionella, have been documented as the infectious pathogens in a significant percentage of nosocomial infections. The diseases associated with legionella infection are legionellosis, frequently resulting in pneumonia, and Pontiac Fever, a less severe illness. The guidance provided in this Section addresses control of Legionella in plumbing systems, and is based in principle on the recommendations found in these references. Typical water supply

systems, including base or public central distribution and local wells, must be presumed to be contaminated with the Legionella bacteria. Standard water utility treatment and testing practices are not considered adequate to ensure protection against the bacteria entering a facility. It is therefore necessary that Legionella bacteria prevention and control guidelines be considered in Medical Treatment Facility designs.

1.2.1 Legionella Characteristics and Transmission. The legionella bacterium is found throughout earth and water (aquifers, wells, reservoirs) environments, and must be expected in all water supplies. The greatest danger to humans occurs when the organism is permitted to multiply or “amplify” in a water supply system to the point that significant numbers of bacteria are present. Factors that lead to amplification include the following:

- Growth support deposits or coatings in system piping or equipment (e.g. scale, sediment, biofilm).
- A water temperature range of 25-42 degrees C (77-108degrees F) of both supply domestic cold and hot water systems, including temperature at fixture discharge, hot water generator, hot water return distribution systems, and in storage or holding tanks.
- Stagnation in tanks, and supply and return distribution systems, for both cold and hot water.

Legionella bacteria become aerosolized in moisture droplets of less than 5 micrometer diameter (optimum transmission droplet size for sustained suspension in air), created by shower heads, faucet aerators, spray nozzles, respiratory equipment, water impacting on hard surfaces, and bubbles breaking (such as occurs in hydrotherapy bath whirlpools). Practical means for altering the aerosols that can lead to legionella infections are limited.

1.3 GENERAL DESIGN CONSIDERATIONS. Legionella protection guidance is provided in applicable locations throughout this Section; however designers should also carefully consider provisions in the latest editions of the guidelines referenced. Healthcare facility

operational procedures for legionella control, such as cleaning or decontaminating of respiratory equipment and environmental sampling, are addressed in the referenced guidelines. The referenced guidelines also address disinfection techniques for reducing Legionella colonization in existing facilities, such as superheated water flushing and hyperchlorination shocking. Generally speaking, the goal of the legionella-protection design is not to eradicate the bacteria, but to prevent or limit colonization.

2. POTABLE WATER SUPPLY SYSTEM.

2.1 QUALITY. All potable water supplies shall have an established potability monitoring program to be acceptable for use by an Medical Treatment Facility. When an Medical Treatment Facility project includes a non-potable water service (i.e., “gray water”) for systems such as irrigation, heating, or cooling, the design shall provide for requirements for signage, pipe labeling, and other means as needed to clearly identify the system (including outlets) as unsafe for human consumption.

2.2 CONTINUITY OF SERVICE. To the extent economically practicable, provide a minimum of two water services for hospitals, with each service fed from separate mains and sources, and designed for full demand (serving potable, process, and fire protection systems). These services should enter the building at separate locations. The purpose of this provision is to provide an uninterrupted supply of potable water, or permit swift service restoration, in the event of a water main break. If two separate water sources are not practically available, on-site storage shall be considered. Where practical, loop the mains around the facility and provide sectionalizing valves.

2.3 BACKFLOW PREVENTION. The flow of non-potable water, or any other nonpotable liquids, into the potable water supply shall be prevented. Necessary measures to prevent backflow, cross connection, or back-siphonage shall be included in the design. Cross connection of a municipal and installation-dedicated (well-based, base pumping station, etc.) system shall require approval from the local Administrative Authorities. Generally, backflow isolation will be required on the main supply mains serving a Medical Treatment Facility; Designers shall coordinate backflow prevention requirements, including

requirements for maintenance accessibility and periodic testing, with the local municipality, as appropriate.

2.3.1 Devices and Methods. All potable water discharge points, such as a faucet discharging into a reservoir sink or tub, shall be provided with an adequate air gap, in accordance with referenced criteria. Fixtures or equipment where the discharge point is positioned below the reservoir rim shall be fitted with a vacuum breaker. Examples of concern include the following:

- Bedpan washers, or similar fixtures including a flushometer valve.
- Flexible-hoses or shower heads, of length sufficient to reach below fixture rim, typically found in procedure rooms, hydrotherapy bath equipment, laboratories, and food service areas (e.g. washers, steam tables).
- Laboratory or other serrated-nozzle fixtures designed to accept flexible tubing.
- Water delivery outlets serving therapeutic, surgical, or autopsy/mortuary procedures.
- Hose bibs.

For the protection of makeup supplies to low hazard equipment (such as autoclaves and fire protection sprinkler systems), double-check backflow preventers may suffice. For the protection of sources supplying high hazard equipment and processes, reduced-pressure backflow preventers are required. Designers shall include provisions for drainage of the discharge from these devices; refer to Tables 1 and 2.

<u>Assembly Pipe Size mm (inch)</u>	<u>Discharge L/s (GPM) at 420 kPa (60 PSI)</u>	<u>Discharge L/s (G/PM) at 1050 kPa (150 PSI)</u>
19- 32 (3/4 -1 1/4)	4.7 (75)	8.8 (140)
38- 50 (1 ½-2)	10.7 (170)	17.6 (280)
63- 75 (2 ½-3)	15.8 (250)	25.2 (400)
100-150 (4-6)	31.6 (500)	53.6 (850)
200-250 (8-10)	33.1 (525)	56.2 (890)

Potential Backflow Preventer Discharge Rates

Table 1

<u>Drain Size mm (inch)</u>	<u>Flow Rate* L/s (GPM)</u>
100 (4)	5.6 (88)
150 (6)	16.8 (264)
200 (8)	36.3 (575)
250 (10)	66.3 (1050)
300 (12)	107.3 (1700)

* Flow rates for a floor drain with slotted cover and 3 mm (1/8 inch) drain pipe slope.

Floor Drain Flow Rates

Table 2

2.3.2 Water Treatment. A water chemistry analysis reporting, as a minimum, the calcium and magnesium concentrations and the water hardness shall be used as the basis for determining the potable water treatment design scope. Water treatment equipment packages requiring regeneration of media or components shall include multiple units as required to permit routine maintenance. Water treatment technologies for the control of waterborne pathogens are discussed below.

2.3.2.1 Scale Control. Water softening will generally be required when the water supply to the facility has a hardness of 170 mg/L (10gr/gal) or more. The softening system should be designed to deliver water with a hardness between 50 mg/L (3 gr/gal) and 85 mg/L (5 gr/gal); designer shall determine if any specialized equipment used in the Medical

Treatment Facility may require more stringent requirements. Dental facilities' water hardness shall not exceed 85 mg/L.

2.3.2.2 High Purity Water Systems. Water purification is the process by which contaminants or impurities, which affect undesirably the performance of specific equipment, or the outcome of medical and laboratory tests, are removed from the water. Water purification systems include reverse osmosis, deionization, ultra filtration, and UV sterilization. Type I and Type III reagent grade water, as specified in ASTM D 1193 (reference 8g), are used in various applications such as for medicine preparation processes in pharmacies, in distillation units, for designated laboratory outlets, and in selected equipment for Renal Dialysis, Glassware Washing, Central Sterile Supply, and other medical and laboratory functions. Their use shall be coordinated with the Using Agency and the Government Design Agent. The designer shall consider local and central treatment options, and treatment system combinations, best meeting the User's needs and overall life cycle cost.

2.3.3 Legionella Control. The relative danger that legionellae pose in any given Medical Treatment Facility is a function of "system" factors which promote or discourage colonization of the relative vulnerability of the patient population, and even of such factors as climate and ground water temperature. The presence of aerosol generating sources such as showers and whirlpool baths increase the risk of legionella infection. More seriously ill patients, particularly those who are immunocompromised by medical condition or treatment, are more vulnerable to legionella infection than the general population. In addition to potential contamination danger from hot water systems, cold water systems pose the risk of supporting legionella colonization if the piping systems are subjected to heat sources. The temperature of cold water systems may be elevated into ranges more conducive to legionella colonization by ground temperatures, piping located in attics, ceiling spaces, equipment rooms, crawlspaces, or other unconditioned spaces, or by being located adjacent to hot water or steam piping. All of these risk factors should be taken into consideration when designing the domestic water system to help determine what special measures, if any, are called for to help control legionella.

2.3.3.1 Scale, Sediment, and Biofilm. Scale, sediment, and biofilm are contaminants that support Legionella bacteria colonization. The extent to which these support colonization is a function of factors including potable water service quality (including the presence of living aquatic amoebae such as are found in biofilms), system operating temperatures, and pipe material. Standard control technologies for scale and sediment deposits normally minimize the contribution of these factors to legionella colonization. Biofilms are resistant to some treatments. For addition and alteration projects, designers must be aware of the potential presence of established biofilms, sediments, and scale. Exercise caution in reusing existing piping system components without an analysis of the existing conditions. It may be contributing to Legionella colonization and subsequently, may lead to contamination of new service.

2.3.3.2 Reducing Legionella Potential in Existing Facilities. High velocity water flushing may be to some degree effective to purge excessive scale and sediment from existing piping or equipment. Additional measures for reducing legionella colonization potential include cleaning or replacement of hot-water storage tanks, hot water generators, faucets, and showerheads. Piping disinfection may be accomplished via hyper chlorination at levels of up to 10 mg/L of free residual chlorine, or by thermal shock (hot water flushing) using water heated to a temperature of 65 degrees C (150 degrees F) or more for a duration of at least 5 minutes.

2.3.3.3 Design Considerations. Treatment systems for legionella control shall be sized on the total potable water demand – both cold and hot. Treatment shall be applied to the water service main. Designs should incorporate the following practices to minimize the potential for legionella colonization:

- Treatment systems shall be provided for hospitals, and shall be either copper-silver ionization or chlorine dioxide.
- Whenever practicable, specify pipe, equipment, and fixture components having direct water contact to be of materials which inhibit bacteria colonization, such as

copper. For inpatient Medical Treatment Facilities, avoid materials that support colonization, such as natural rubbers and some plastics, whenever practical.

- Design distribution mains to maintain balanced flow throughout. Piping runs should be as short as practicable. Avoid creating piping “zones” which experience infrequent use, and therefore stagnation. As practicable, route mains close to fixtures to minimize the lengths of branch piping runs. Avoid creating stagnant piping sections, e.g. dead legs. Do not locate cold water piping near hot water piping or other heat sources.
- Locate pressure balancing and thermostatic mixing anti-scald valves as close as practicable to the fixture discharge. The maximum pipe run should be 2 meters (6 feet).
- Piping between fixture shutoff and discharge should be self-draining where possible.
- Use care to properly select the operating head of the recirculation pump(s), taking into consideration system head requirements, including the pressure drop of thermostatic mixing valves.
- Consider instantaneous hot water generators where feasible, and when on-site storage is not required by other criteria, to avoid stagnant storage conditions.
- Water storage of holding tanks, both cold and hot, shall be designed to have continuous flow with maximum practical velocity. They shall not be piped as branched components with discharge line shutoff valves closed. Storage tank capacity shall be adequate for the application, but not oversized. The capacity sizing shall factor in the current healthcare procedures such as increased outpatient medical functions reducing the load profiles and hot water recovery demand.

2.4 DOMESTIC HOT WATER SYSTEMS.

2.4.1 Hot Water Demand. The demand load can be calculated using several different methods, examples of which are contained in ASHRAE and American Society of Plumbing Engineers (ASPE) handbooks. The preferred method for calculating hot water demand for a Medical Treatment Facility is the per-fixture method. This method provides a means to account for various uses within each facility, and permits the tabulation of the hot water load using a specified demand for each fixture. Summing individual fixture demands, the total demand is utilized to size the heater recovery rate and storage size. Table 3 provides a list of representative fixtures and their demands based on data provided in ASHRAE and ASPE handbooks.

FIXTURE	<u>L/H</u>	<u>(GPH)</u>	<u>HW</u> <u>SFU</u>
Sink, Clinic	15	(4)	3
Sink, Plaster	38	(10)	3
Sink, Service (General)	76	(20)	3
Lavatory, Public (General)	23	(6)	1½
Lavatory, Patient (Private)	8	(2)	1
Lavatory, Clinic	30	(8)	3
Basin, Mop Service	76	(20)	3
Shower, Staff or Patient Group	284	(75)	3
Shower, Patient (Private)	114	(30)	2
Shower, Hydrotherapeutic	1520	(400)	11
Bathtub	76	(20)	3
Bath, Whirlpool, Arm	130	(35)	3
Bath, Whirlpool, Arm/Foot/Knee	57	(15)	3
Bath, Whirlpool, Leg	380	(100)	7
Bath, Body Hydrotherapy (Hubbard)	2270	(600)	17
Bath, Sitz 114 (30) 3			
Processor, X-ray	57	(15)	3

Table 3

For any fixture not shown, the designer shall determine the demand rate based upon experience, standard practice, and available Using Agency input. An example of system sizing is given below:

Example 1: Determine the heater and storage tank size for a medical clinic with the following fixture schedule:

12 Clinic Sinks	X	15.0 L/h	{ 4 gph }	=	180.0 L/h	{ 48 gph }
1 Plaster Sink	X	38.0 L/h	{ 10 gph }	=	38.0 L/h	{ 10 gph }
8 Public Lavatories	X	23.0 L/h	{ 6 gph }	=	184.0 L/h	{ 48 gph }
12 Clinic Lavatories	X	30.0 L/h	{ 8 gph }	=	360.0 L/h	{ 96 gph }
2 Mop Service Basins	X	76.0 L/h	{ 20 gph }	=	152.0 L/h	{ 40 gph }
1 Arm Whirlpool Bath	X	130.0 L/h	{ 35 gph }	=	130.0 L/h	{ 35 gph }
1 Leg Whirlpool Bath	X	380.0 L/h	{ 100 gph }	=	380.0 L/h	{ 100 gph }
1 Foot Whirlpool Bath	X	57.0 L/h	{ 15 gph }	=	57.0 L/h	{ 15 gph }
1 X-ray Film Processor	X	57.0 L/h	{ 15 gph }	=	<u>57.0 L/h</u>	<u>{ 15 gph }</u>

Possible Maximum Demand 1538.0 L/h (407 gph)

Using the Demand Factor of 0.40 yields

Probable Maximum Demand = Possible Maximum Demand X Demand Factor
 Recovery Rate = 1538.0 L/h X 0.40 (407 gph X 0.40)
 Heater or Coil Capacity = 617.4 L/h (162.8 gph)

The Storage Capacity Factor of 1.00 is then applied to this recovery rate or heater capacity to determine the

Storage Tank Capacity = Heater Capacity X Storage Capacity Factor
 = 617.4 X 1.00 (162.8 X 1.00)
 = 617.4 L (162.8 gal)

Explanation of Example 1:

A Demand Factor is applied to the Possible Maximum Demand to calculate the Probable Maximum Demand. The Probable Maximum Demand is the rate at which the heater shall generate hot water, or the recovery rate.

The Probable Maximum Demand is factored by the Storage Capacity Factor to determine the Storage Tank Capacity. The Storage Tank Capacity is the capacity required being available for use. Storage tanks are not considered to be 100% usable and thus, a usable storage tank factor shall be applied to the calculated storage tank capacity; the percent capacity considered usable for most tanks is 70, thereby resulting in a 1.43 usable storage tank factor. The usable storage tank factor for systems utilizing instantaneous generators or multiple tank arrangements shall be coordinated with the occupant.

Additional Note: The fixture-unit method is adequate for typical usage.

Expanded usage for food service, non-standard fixtures, or abnormal usage patterns (extreme low or high demand peaks or erratic peak duration and

occurrence) shall be factored into the sizing calculations. For example, food-service fixture demand factors need to be adjusted if disposable service ware is used. Concentrated patient treatment for sick call, or other instance of high-peak usage, is another example of fixture hot water demand adjustment.

The Demand Factor and Storage Capacity Factor are listed in References 8h and 8i for given building types, which include a hospital but not medical clinic, dental clinic, nor laboratory. A Demand Factor of 0.40 and Storage Capacity Factor of 1.00 are considered representative for a clinic upon review of the factors for the building types shown. Factors for Medical Treatment Facilities with laboratory space greater than 10% of the total facility space shall be coordinated with the user.

2.4.2 Hot Water Design Temperature. Domestic hot water shall be generated and stored at 60 degrees C (140 degrees F) minimum. It shall be tempered with a thermostatic mixing valve at the hot water generator discharge to permit distribution at a temperature range between 43 and 52degrees C (110-126 degrees F). The maximum hot water temperature distribution design set point shall be 43 degrees C (110 degrees F).However, provide the capability to increase system temperature to 52degrees C (126 degrees F) to permit a Medical Treatment Facility the option to increase the temperature if so recommended by the Infection Control Officer. It is extremely important to note that at this temperature the exposure time for a first-degree burn is approximately 45 seconds. This is considered an adequate period for a fully aware adult to remove the exposed body area from the stream of a sink or lavatory, thereby maintaining a relatively safe condition at these fixtures without the requirement furan anti-scald valve. Infants, persons desensitized by medical condition or treatment, or those with severely limited motor capabilities, may be endangered by water at this temperature. Anti-scald valves shall be provided as close as possible to the taps of “whole-body” fixtures such as showers, bathtubs, and hydrotherapy baths. Hot water recirculation systems shall be designed to limit system temperature drop to 3 degrees C (5.5 degrees F) or less. Maximum hot water temperatures for other applications shall not exceed the following:

- Supply and Utility Areas. Central sterile supply, soiled utility rooms equipped with bedpan washers, cart wash areas, and special pathological wash areas shall be provided with 60 degrees C (140 degrees F) hot water.
- Kitchen Areas. The temperature normally required in dietary areas is the same as that distributed to standard hand washing and bathing plumbing fixtures. Dishwashing (automatic equipment) and pot washing normally require 82 degrees C (180 degrees F). Booster heaters shall be provided to obtain this temperature.
- All Other. All other domestic hot water applications shall be provided with a hot water temperature the same as is distributed to standard hand washing and bathing fixtures.

2.4.3 Hot Water System Temperature Maintenance. In most facilities, a means of controlling system heat loss (and therefore temperature decrease) will be required to maintain delivery temperatures within acceptable tolerances. Hot water recirculation is required for all patient care facilities (both inpatient and outpatient), and shall be located as close to the fixture connections as practicable. Designs shall include provisions for isolating and balancing the system. Heat tape systems may be utilized in non-patient care facilities if cost justified, but are considered less desirable due to reported system malfunctions and difficulty in locating the malfunction point.

2.5 PLUMBING FIXTURES AND OTHER EQUIPMENT. Plumbing fixtures should conform generally to American Society of Mechanical Engineers International, ASME standards series A112 or International Association of Plumbing and Mechanical Officials, IAMPO standards series Z124.

2.5.1 Handicapped Fixtures. Provide handicapped fixtures in accordance with the requirements of the Accessibility Provisions for the Disabled Section of this document and the TMA PFD.

2.5.2 Drinking Water Coolers. Locate public drinking water coolers convenient to each public waiting room and elsewhere as directed. The standard rating and performance shall conform to ARI Standard 1010 (reference 8m). Refer to the Accessibility Section of this document for handicapped requirements.

2.5.3 Emergency Shower/Eye Wash Fixtures. Design in accordance with the American National Standards Institute (ANSI) Standard Z358.1.

2.5.4 Water Usage Conservation. As of July 1992, the National Energy Policy Act (EPACT) has specified maximum consumption requirements for water closets, urinals, faucets and shower heads (for example, the water closet standard was lowered from 13.2 liters (3.5 gallons) per flush to 6.1 liters (1.6 gallons)). Low-flow fixtures shall be specified for all projects.

2.6 SANITARY DRAINAGE SYSTEM. The Medical Treatment Facility sanitary waste system shall be connected to an approved existing sewer system, either government or private as appropriate. If an existing sewage disposal system is not available, an approved alternative system shall be provided. For example, a holding tank may be acceptable for remote locations, for temporary service while awaiting the installation or retrofit of an approved sewage disposal system, or a backup such as for hardened or essential facilities. Any alternative to an approved central sanitary system shall be coordinated with the Installation's local approving authority. When connected to a local public system, code requirements in excess of the IPC (reference 8b) imposed by the local regulatory agencies shall be considered in the design. The system shall be designed to avoid excessive back pressure and aspiration effects. Adequate cleanouts shall be provided to permit access to all sections of the waste drainage system. The cleanouts shall be located to avoid or minimize disruption of medical functions. If a facility sanitary waste requires lifting or pumping, provide duplex pumping equipment and a backflow preventing check valve. This equipment shall be connected to the alternative power source if one exists, or is included in the project scope.

2.6.1 Protection of Special Fixtures and Equipment. Fixtures and equipment used for sterilization, and food preparation, processing, or storage, shall be protected from

contamination by backflow of waste. An indirect waste line, such as an air break or physical disconnection (open drain) at the associated waste outlet, shall be incorporated into the system design. These provisions also apply to equipment that cannot be easily cleaned. Included are sterilizers, glass washers, refrigerators, kitchen equipment, film X-ray processors, dental lab equipment (e.g. boilout assembly tanks), and vacuum system separator tanks.

2.6.2 Special Drainage Equipment. Interceptors shall be provided when precious materials or heavy metals, such as silver and barium, are sediment in the waste drainage from such spaces as a Cast Room, a Prosthodontics Laboratory, barium procedure areas, film X-ray processing, and spaces employing blood analyzers. Interceptors for barium waste shall be aluminum. Flush rim floor drains shall be provided in Autopsy. Garbage grinding disposers shall be provided in kitchens on dishwashers, pot and pan sinks, and other sinks as designated. Grease traps shall be provided with grease-producing kitchen equipment including prewash sinks, pot washers or sinks, and floor drains serving kettles. Separators shall be provided in uses where petroleum products are subject to dripping or spills, such as ambulance garages and mechanical equipment rooms.

2.6.3 Special Purpose Waste Lines. Separate waste lines shall be provided for acid waste and radioactive waste from laboratories, darkrooms and nuclear medicine treatment rooms, when justified by the quantities and/or concentration of reagent expected to be introduced. Acid-resistant waste piping will be utilized for such applications and, if required, will pass through a neutralizing or dilution tank before combining with building waste. If large quantities of acid or strong base solutions are to be discharged into the waste system, neutralization will be required. There are various radioactive materials to be found in a Medical Treatment Facility. The particular radioactive waste for a given facility shall be identified. The appropriate prescribed manner of disposal in accordance with federal and local safety standards shall be incorporated into the design.

2.6.4 General-Purpose Floor Drains. General floor drains shall be considered for rooms in which water-using plumbing fixtures or equipment are located. These include physical therapy rooms which are equipped with hydrotherapy equipment, central sterile areas for

sterilizers and sanitizing washers, food service areas, wash-down and housekeeping. Floor drains are normally not required at emergency shower locations.

2.6.5 Trap Priming. Where a trap seal is subject to loss by evaporation, a trap seal primer valve shall be installed per IPC. When utilized, automatic primers shall incorporate a backflow prevention feature. Other means of trap prime maintenance, such as using alternative sealing fluids (e.g. glycerin), are not permitted.

2.6.6 Retrofit/Alteration Considerations. The replacement of older existing fixtures with lower-flow fixtures will alter system performance. Smaller diameter pipe or increased slope may be necessary alterations.

2.6.7 Elevator Pit Sumps. Elevator pits shall be provided with a sump, which shall be either pumped or drained by gravity. Pumped designs shall deliver fluids to an indirect connection to the sanitary or storm drainage systems, such as a floor drain. The sump discharge line shall include a check valve to prevent back flow of fluid into the sump. If permitted by the local jurisdiction, a direct connection to the storm drainage system may be considered. Designers should also determine from the base engineering office or local jurisdiction if an oil interceptor is required. No other drains or sump discharges shall be connected to the elevator pit drain or sump. This equipment shall be connected to the alternative power source if one exists or is included in the project scope.

2.6.8 Mercury Control. Facilities containing operations which generate mercury wastes in the free or leachable (e.g. dental filling amalgams) state which are intended to be disposed to the sanitary waste system, shall consider separation provisions in accordance with federal, state or local requirements. The separation provision shall be incorporated as close to the source point as feasible. For mercury generating operations which do not require a separation provision initially, provide a 0.2 square meter (2 square foot) floor space with 0.67 meter (2 foot) clearance all around to accommodate a retrofit installation.

2.7 STORM WATER DISPOSAL. Provide drainage and disposal of storm water, direct or from runoff, from roofs and paved areas. The means of disposal shall preferably be to an existing storm sewer. If an existing storm sewer of sufficient capacity is unavailable,

alternative means of disposal, including such options as ponds, basins, or dry wells, shall be considered. Storm water disposal shall be consistent with the Installation's storm water management plan.

2.7.1 Prohibited Discharge. Storm water shall not be discharged into sanitary sewers, unless it is rated as a combination system and no alternative cost-effective means is available. When storm water is discharged into a combination system, the connection at the point of combining with the sanitary waste shall include a trap.

2.7.2 Sizing. Sizing of the storm water drainage system shall be based on the guidance and precipitation rates shown in the IPC. When approved, local storm data may be utilized if based on U.S. Weather Bureau specified sampling methods.

2.8 FUEL GAS SERVICE. Applications for fuel gas utilization in Medical Treatment Facilities include fuel source for space heating, domestic hot water generation, cooking, generation of steam for humidification and sterilization, and as a point-of-use heat or flame source to support medical and laboratory functions. The gas service for medical and laboratory functions is discussed below. Fuel gas system design, including liquefied petroleum gas systems, shall be in accordance with NFPA 54, 58, and 59A as applicable.

2.9 MEDICAL GAS SYSTEMS. Medical gas systems include: compressed air for medical and dental patient and laboratory use; vacuum for medical and dental patient use, laboratory dust collection, waste anesthesia gas disposal; and gases for patient, laboratory, and equipment use. See Table 4 for general information. Medical gas systems shall be designed to be safe, reliable, and maintainable.

Compressed Air -----	Notation	Nominal Description
Medical Compressed Air	MCA	345-380 kPa (50-55 psig)
Dental Compressed Air	DCA	620-655 kPa (90-95 psig)
Laboratory Air - Dental	LA	210-245 kPa (30-35 psig)
Laboratory Air - Medical	LA	345-380 kPa (50-55 psig)
Process Air	PA	830-865 kPa (120-125 psig)
Vacuum		
Medical Vacuum	MV	51-65 kPa (15-19 in-Hg)
Dental High Vacuum	DHV	51-65 kPa (15-19 in-Hg)
Dental Low Vacuum	DLV	21-27 kPa (6-8 in-Hg)
Laboratory Dust Evacuation	LDE	10 kPa (3 in-Hg)
Waste Anesthesia Gas Disposal	WAGD	21 kPa (6 in-Hg)
Oxygen	OX	345-380 kPa (50-55 psig)
Nitrous Oxide	NO	345-380 kPa (50-55 psig)
Nitrogen	NI	1100-1275 kPa (160-185 psig)

Table 4

2.9.1 Systems for Medical Clinics. Centrally piped medical gas/air/vacuum systems are not normally required or authorized for outpatient medical treatment clinics. If attached to an existing facility having central systems, Designers shall consider extending service lines to the clinic if life cycle cost effective.

2.9.2 Dental Clinics. Centrally piped systems shall normally be provided for dental compressed air (DCA), low volume oral evacuation (DLV), high vacuum oral evacuation (DHV), high volume evacuation for laboratory dust use (LDE); dental laboratory air (LA), and surgical hand piece drive air (SHDA) as required to support the planned functions. A separate system for Waste Anesthesia Gas Disposal (WAGD) may be required unless the Using Agency designates the DHV or DLV system for that purpose. Fuel gas (natural or propane) shall be provided as required to support prosthodontic and orthodontic laboratories and Dental Treatment Rooms (DTR's). For freestanding clinics with less than 5 chairs, selection of central system for gases as opposed to point-of-use systems shall be based upon life cycle cost considerations.

2.9.3 System Control Valves. All medical gas centrally piped systems shall be provided with shut-off valves and zone valve box assemblies in accordance with NFPA 99. Additional shutoff valves shall be included as necessary to provide system section isolation for maintenance or alterations.

2.9.4 Alarm Systems. Medical gas alarm systems shall be provided for all central piped systems in accordance with NFPA 99.

2.9.5 Gas System Sources (Storage). Gas system sources or storage provisions shall be designed in accordance with NFPA 99. Flammable and nonflammable storage containers shall be stored in separate enclosures. Bulk oxygen storage design shall be in accordance with NFPA 50.

2.9.6 Point-of-Use Sources. Point-of-use cylinders are defined as B, D, or E sizes. The Designer shall coordinate with the Using Service the provisions for point-of-use cylinder storage when their use is planned. Storage in the storage room for central system cylinder banks is permissible. The point-of-use cylinder volume shall be included in the total when determining the storage room ventilation requirements. Design shall incorporate Compressed Gas Association requirements of Pamphlet P-2.

2.9.7 Alternative Compressed Air Sources. Alternative compressed air sources such as pneumatic control air or shop air compressors shall not be used as a source for medical compressed air, dental compressed air, laboratory air, process air, or surgical hand piece drive air.

2.9.8 Color Coding and Labeling. Labeling and color identification of piping shall be in accordance with NFPA 99 and the CGA Pamphlet C-9. System components shall also be labeled for identification to prevent tampering and inadvertent closing. In particular, shutoff valves and pressure gauges shall be labeled in accordance with NFPA 99.

2.9.9 Medical Gas Systems Outlets. The Designer shall coordinate the gas types and outlet quantities with the Using Service. Additional outlets and gas types may be provided when justified by the Using Service to TMA. All outlets shall comply with the latest edition of

NFPA 99 and the requirements of Compressed Gas Association Pamphlet V-5. There are DISS and Quick Connect type outlets, with two primary different configurations of the Quick Connect outlet. Therefore, designer shall also coordinate the outlet type configuration with the Using Service so that the Users will not have to use an outlet adapter for their existing medical equipment.

2.9.9.1 Outlets for Non-Medical Function Use. The use of a central medical gas system to serve an outlet that indirectly supports the medical function such as in a laboratory may be justified. If so, the branch piping and outlets shall be in accordance with NFPA 99. Non-medical uses are not permissible except for unique circumstances with documented waiver requests, coordinated with the user, reviewed individually.

2.9.10 Emergency Power Source. Life-critical medical gas system equipment, requiring electrical power for generation, operation, or alarm, shall be connected to an emergency power source. At the discretion of the designer, when requested by the user, dental compressed air, vacuum, and medical gas systems serving anesthetizing treatment rooms in outpatient and dental treatment clinics may be connected to an emergency power source.

2.9.11 Medical Compressed Air (MCA). The MCA system shall be an independent central piped system consisting of two or more medical air compressors and a central receiver, all conforming to the requirements of NFPA 99. It shall be used only for medical functions requiring breathable air to support respiration or for air-driven instruments that discharge into the pharynx. The MCA system shall not be used to satisfy any other compressed air requirements. The system design shall include automatic operation of the compressors, including alternating lead/lag status.

2.9.11.1 Air Quality Standards. The medical air compressor(s) shall be specifically designed and manufactured for this purpose. MCA quality shall be as defined in NFPA 99 (reference 8r). Intake air shall be direct from outdoors or another source of equal or better quality located in accordance with NFPA 99. Designers are responsible to size and show routing of medical air intake piping.

2.9.11.2 General Requirements. MCA shall be provided by two or more compressors with provisions for automatic, alternating, and simultaneous operation. The compressors shall be sized such that if any one compressor fails, the remaining compressor(s) shall provide 100% of maximum system demand. Provide an alarm to indicate compressor failure that annunciates at the master medical gas alarm panel. All system components downstream of the compressors shall be sized for 100% standard system demand and be duplexed. The receiver shall have an automatic drain feature specified

2.9.11.3 Air Drying. System design shall include an air dryer of either the mechanical refrigeration or desiccant type. Designers shall closely coordinate with the Using Agency for each project, to determine whether operating conditions, facility maintenance capabilities, air dryness limitations, or other factors favor preference of one type over the other for the given application. Designers are responsible to consider the following:

- When mechanical refrigeration systems are specified, designers shall include specification of a cycling feature for all systems under 3.7 kW (5 horsepower (hp)), to minimize the possibility of icing and moisture carry-over. Designers shall evaluate whether anticipated flow conditions will require the cycling feature for systems 3.7 kW (5 hp) and over.
- When desiccant systems are specified, designers shall consult the Using Agency on dryness limitations. Desiccant dryers are capable of drying the air to a dewpoint as low as –40 degrees C (-40degrees F), which may be considered too low for some medical or dental applications. When required by the User, the design shall include specification of equipment accessories that will permit upward adjustment of air moisture to the required dewpoint.
- The relative advantages and disadvantages of mechanical refrigeration dryers and desiccant dryers generate questions. Good arguments may be made for in favor of either dryer type. Both systems can be successfully utilized in Medical Treatment Facilities if project-specific conditions and User needs are taken into account and the equipment is properly specified.

2.9.11.4 MCA Demand. System demand shall be calculated utilizing the peak flow and simultaneous use data in Table 8-5, as a minimum. The simultaneous use factors shall be used with judgment and modified to adapt to special conditions if required.

<u>Space/Equipment</u>	<u>Per Unit</u>	<u>Design Flow in L/s (SCFM)</u>			<u>Usage Factor %</u>
		<u>Per Room</u>	<u>Per Bed</u>	<u>Per Outlet</u>	
Anesthetizing Locations:					
Special Surgery & Cardio-Vascular			0.2(0.5)		100
Major Surgery & Orthopedic		0.2(0.5)			100
Minor Surgery		0.2(0.5)			75
Emergency Surgery		0.2(0.5)			25
Radiology		0.2(0.5)			10
Cardiac Catheterization		0.2(0.5)			10
Ventilators	1.7(3.5)				100
Delivery Room		0.2(0.5)			100
Acute Care Locations:					
Recovery Room/Surgical			0.9(2.0)		25
ICU/CCU			0.9(2.0)		50
Emergency Room			0.9(2.0)		10
Neonatal ICU			0.7(1.5)		75
Dialysis Unit			0.2(0.5)		10
Recovery Room/O.B.			0.9(2.0)		25
Subacute Care Locations:					
Nursery		0.2(0.5)			25
Patient Rooms		0.2(0.5)			10
Exam & Treatment	0.5(1.0)				10
Pre-Op Holding				0.7(1.5)	10
Respiratory Care	0.5(1.0)				50
Pulmonary Function Lab				0.5(1.0)	50
EEG & EKG				0.5(1.0)	50
Birthing & Labor/Delivery	0.5(1.0)				50
Other:					
Anesthesia Workroom		0.7(1.5)			10
Respirator Care Workroom	0.7(1.5)				10
Nursery Workroom		0.7(1.5)			10
Equipment Repair		0.7(1.5)		0.7(1.5)	10
Med. Laboratory				0.7(1.5)	25

Medical Compressed Air System Demand

Table 5

2.9.12 Dental Compressed Air (DCA). A central piped dental compressed air (DCA) system with two or more compressors and other components described herein shall be provided in accordance with NFPA 99, Level 3 compressed air systems. DCA shall be used for drying applications during dental procedures and as a power or drive source for lifts, locks, and pneumatic dental instruments and equipment. DCA, unlike MCA, is not used for breathing or respiratory support of any kind and shall not be used to satisfy MCA

requirements. Air that is normally used for dental laboratory restorative and fabrication techniques may be provided by the DCA system.

2.9.12.1 Air Quality Standard. DCA quality shall be as defined in NFPA 99, Level 3 compressed air systems. Intake air shall be direct from outdoors or of quality better than outside air.

2.9.12.2 DCA Components. DCA shall be provided by two or more equally sized compressors, with provisions for automatic, alternating, and simultaneous operation. Each compressor shall be sized such that if anyone compressor fails, the remaining compressor(s) shall provide 65% of standard demand. Provide an alarm to indicate compressor failure that annunciates to the master medical gas alarm panel. All system components downstream of compressors shall be sized for maximum combined compressor output. In-line pressure regulators shall be provided when DCA and dental LA systems are served by a common compressor. Each laboratory supply main shall have a pressure regulator. Dryer type may be of either the mechanical refrigeration or desiccant type, according to project specific operational requirements and the User's needs.

2.9.12.3 DCA System Demand. The system shall be sized using the following criteria:

a. Select a DTR Usage Factor:

<u>Number of DTR's</u>	<u>DTR Usage Factor (DUF)</u>
1-3	1.0
4-6	0.9
7-12	0.8
13-19	0.7
20 and up	0.6

b. DTR Demand = No. of DTR's X 1.42 L/s X DUF

c. Select a lab usage factor:

<u>Number of Technicians</u>	<u>Lab Usage Factor (LUF)</u>
1-5	0.6
6-10	0.5
11-19	0.4
20 and up	0.3

d. Lab Demand =

- No. of Technicians X 0.472 L/s X LUF
- + No. of sand/shell blasters X 1.288 L/s X LUF
- + No. of air chisels X 1.415 L/s X LUF
- + No. of denture presses X 0.472 L/s X LUF
- + No. of microblasters X 2.831 L/s X LUF
- + No. of high speed hand pieces X 1.415 L/s X LUF

e. Sterilization demand = No. of hand piece purge stations X 0.472 L/s.

f. Standard demand = DTR demand + Lab demand + Sterilization demand.

g. Select the optimum compressor grouping:

COMPRESSOR GROUPING

<u>Type</u>	<u>System Usage Factor (SUF)</u>
Duplex	0.65
Triplex	0.33
Quadplex	0.25

h. Compressor size = SUF X Standard demand

<u>Number of DTR's</u>	<u>Liters (Gallons) per DTR</u>
1 -6	34(10)
7 -9	30(9)
10 – 12	26(8)
13 - 15	23(7)
16 - 18	19(6)
19 - 21	15(5)
Over 21	15(4)

Receiver Size

Table 6

2.9.13 Laboratory Air (LA). The medical or dental laboratory air (LA) system shall be a central piped system consisting of two or more compressors and a central receiver, all conforming to the requirements of NFPA 99.

2.9.13.1 Air Quality Standard. Air compressors used for LA shall be specifically designed and manufactured for this purpose. LA quality shall be in accordance with the dental compressed air (DCA) requirements defined above. Intake air shall be direct from outdoors or of quality better than outside air (e.g., profiteered outdoor air or relieved return air). Locate intake in accordance with DCAs requirements as defined in NFPA 99, Level 3. LA shall be supplied at a minimum of 210 kPa (30 psig) for dental laboratories and 345 kPa (50 psig) for medical laboratories, with a +35 kPa (5 psig) tolerance.

2.9.13.2 LA System Components. LA shall be provided by two equally sized compressors with provisions for automatic, alternate, and simultaneous operation. Each compressor shall be sized to provide 65% of maximum demand. Provide an alarm to indicate compressor failure that annunciates to the master medical gas alarm panel. All system components downstream of compressors shall be sized for maximum combined compressor output. A DCA compressed air generator package used to service a LA system shall be supplied by a

dedicated main located just downstream of the final package component and inside the equipment room.

2.9.13.3 LA System Demand. The LA system flow demand shall be determined by the number of work stations and their function plus the requirements for laboratory equipment. The user shall provide this information. The designer in conjunction with the user shall establish the flow rates. Medical LA system flow rate demand shall be 0.5 L/s (1 cfm) per outlet. Dental LA system flow rate demand is determined by the sizing procedure shown. The simultaneous use factors shall be as follows in Table 7:

<u>No. of Outlets</u>	<u>Use Factor</u>	<u>Minimum L/s (CFM)</u>
1-2	100	
3-12	80	1.4 (3)
13-38	60	4.7 (3)
39-115	40	11.8 (25)
116-316	30	23.6 (50)
317-700	20	44.8 (95)

Medical Laboratory Air System Demand

Table 7

2.9.14 Instrument Air (IA). An Instrument Air (IA) system is intended to be used to power medical devices not related to human respiration (e.g. to power surgical tools, surgical arms, and surgical columns). This system may be utilized in lieu of a high pressure piped nitrogen (NI) system. The user in conjunction with the designer will identify IA requirements. IA shall not be used to satisfy Medical Air (MA) requirements. IA systems shall be designed in accordance with the requirements of NFPA 99.

2.9.14.1 Air Quality Standard. Air compressors used for IA shall conform to the requirements of NFPA 99. Instrument air quality shall be as defined in NFPA 99 (reference 8r). It is recommended that intake air be direct from outdoors, but it is permitted to be within the equipment room.

2.9.14.2 IA System Components. The number of compressors for an IA system shall be a function of the application; however, at least two compressors or one compressor with a

standby header must be provided as a minimum. Coordinate the compressor arrangement with the user. Each compressor shall be sized to provide 100% of the demand. Provide an alarm to indicate compressor failure that annunciates to the master medical gas alarm panel in accordance with NFPA 99. All system components downstream of compressors shall be sized for 100% of the system peak demand.

2.9.14.3 IA System Demand. The number of workstations and their functions plus the requirement of any equipment shall determine the IA system flow demand. The user shall provide this information. The designer in conjunction with the user shall establish the flow rates.

2.9.15 Surgical Handpiece Drive Air (SHDA). SHDA may be used as a substitute for nitrogen to power pneumatic surgical handpieces used in dental procedures. SHDA is not used for breathing or respiratory support. SHDA must be a separate system from DCA and dental LA; however, DCA may be used as a first stage of compression.

2.9.16 Medical-Surgical Vacuum System (MV). The medical vacuum (MV) system shall be a centrally piped, dry vacuum system containing two or more continuous duty pumps with a central receiver. The system shall meet the requirements of NFPA 99 and shall be sized so that if one pump fails, the remaining pump(s) can supply 100% of the total system demand. The system design shall include automatic operation of the vacuum pumps including alternating lead/lag status. Provide an alarm to indicate vacuum pump failure that annunciates to the master medical gas alarm panel.

2.9.16.1 Applications. The MV shall be used only for medical functions involving patient care, therapy, and diagnostic functions as described below. It may also serve DHV requirements for dental treatment rooms and oral surgeries, and small laboratories in patient care areas that function in direct support of medical functions. Analysis, research or teaching laboratory located within a Medical Treatment Facility may also be served by the MV, provided that a separate system connection or main is provided at the vacuum receiver, with a shutoff valve and trap with a drain valve. A laboratory not supporting medical functions shall have a vacuum system separate from the MV.

2.9.16.2 Demand. Vacuum system pumps and piping shall be sized in accordance with NFPA 99 "Recommended Vacuum Source Sizing" and "Recommended Minimum Pipe Sizing." Note to "round up" pipe sizes, especially those serving operating rooms including the risers and laterals. Ascertain the intended staff operational procedures to determine the need for an additional factor of safety. Indiscriminate opening of vacuum inlets for extended periods, whether in service or not, requires a factor increase in demand and pipe sizing. Also, the intended use of "Y-connectors" as a means of increasing available inlets is not recommended. A justified need for a vacuum inlet shall be accommodated with another wall inlet, not a Y-connector. Verify with the User's representative that the number of vacuum inlets proposed will support the planned medical function operation without the use of Y-connectors.

2.9.16.3 Performance. System pressure drop shall be a maximum of 10 kPa (3 in-Hg) at the calculated demand flow rate. A flow rate of 1.4 L/s (3 scfm) per inlet, with no equipment attached, shall be measured while maintaining 41 kPa (12 in-Hg) vacuum at the farthest inlet. The 1.4 L/s (3 scfm) without equipment is equivalent to the recommended 0.7 L/s (1.5 scfm) with.

2.9.16.4 Slide Brackets. Vacuum bottle slide brackets shall be provided for all medical vacuum inlets. Vacuum bottles shall be used at all vacuum inlets to prevent liquids and solids from entering the piping network. Vacuum bottles shall be provided with an overflow shut-off device to prevent carry over of fluids or solids into the piping system. Brackets shall be positioned to provide proper clearance for flow meters and adapters and to eliminate conflict with electrical receptacles. Thus, it is recommended that the vacuum outlet be located at either end of a group of medical gas outlets, with the slide bracket to the outside, e.g. in a healthcare station head wall unit. If two vacuum inlets are required at a given station, locate one at each end of the outlet group with the slide brackets to the outside. It is critical to coordinate vacuum inlet and slide locations with the Architectural Designer and the User's representative to avoid interference with other items without compromising the medical function.

2.9.16.5 Vacuum shall be exhausted in accordance with NFPA 99.

2.9.17 Dental High Vacuum (DHV). A central DHV system may be supplied for areas in dental clinics where MV is required. This system is also a dry system with a central piped distribution system and receiver; no liquids or solids shall be transported in the distribution system. Individual separators shall be located in each applicable DTR. The system shall consist of two or more vacuum pumps and a central receiver. System shall be sized so that upon failure of one pump the remaining pump(s) shall maintain the minimum vacuum specified while providing 100% of the calculated demand. The system design shall include automatic operation of the vacuum pumps including alternating lead/lag status. Provide an alarm to indicate vacuum pump failure that annunciates to the master medical gas alarm panel. For dental clinics located in a hospital, the MV system may be used in lieu of a DHV system.

2.9.17.1 Performance. A minimum vacuum of 65 kPa (19 in-Hg) shall be maintained at the receiver. System pressure drop shall be such that the most remote inlet will have a minimum vacuum of 41 kPa (12 in-Hg) under peak demand conditions. System pressure drop shall be a maximum of 10 kPa (3 in-Hg) at the calculated demand flow rate.

2.9.17.2 Demand. System demand shall be calculated based on 0.9 L/s (2 SCFM) for each DTR DHV inlet with the demand factors in Table 8:

<u>No. of DTR DHV Inlets</u>	<u>Use Factor</u>
1 – 6	1.0
7 – 10	0.8
Over 10	0.6

DHV Demand Factors

Table 8

2.9.18 Dental Low Vacuum (DLV). A central low vacuum, high volume oral evacuation system or DLV shall be installed in dental clinics to provide scavenging, collection, and disposal of liquids, solids, and aerosols from dental procedures. This is a wet system with liquids and solids transported through wetted piping from the collection point to one or more liquid/air separator tanks located upstream of two or more vacuum pumps. The tank serves

as a collector for the fluids and solids and provides a means of automatic draining for them by being connected, indirectly, to the sanitary sewer. The tank draining system may include an automatic wash down feature for larger systems in a Medical Treatment Facility having greater than 10 DTR's. The system shall meet the requirements of NFPA 99, Level 3 vacuum systems. The vacuum pumps shall be sized so that when one pump is inoperable, the remaining pump(s) shall provide the above vacuum pressure and fluid flow for a minimum of 70% of the system demand. The system design shall include automatic operation of the vacuum pumps including alternating lead/lag status. Provide an alarm to indicate vacuum system fault (e.g. pump failure) that annunciates to the master medical gas alarm panel. Protocol shall include alarm initiation when a pump does not operate when called for and when a pump operates when not called for.

2.9.18.1 Components. The service inlet normally is floor mounted in a utility center at the dental chair, or wall mounted with a means of connection to clinical end items such as the high volume hose. The separator(s) shall receive all liquid, air, and solids upstream of vacuum pump(s). Liquids and solids shall be discharged from the separator(s), with piped gravity flow through an air gap into a trapped and vented receptor (e.g. a floor drain or sink, or standpipe receptor for small system suspended tank installations) connected to the sanitary waste system. Local codes may require the use of an amalgam separator between the separator tank and the sanitary waste system to control the discharge of mercury into it. Coordinate with the Ins local regulatory agency when discharge is to a public sanitary system. The separator tank shall discharge a minimum of once during a 24-hour interval for a one-tank system, when a high liquid level sensor activates for a two-tank system, or multiple daily discharges as recommended by the manufacturer. Separator overflow protection shall be included to protect during periods of abnormal usage or when the automatic discharge malfunctions.

2.9.18.2 Performance. The system operating range shall be 21 to 27kPa (6 to 8 in-Hg). A minimum vacuum of 21 kPa (6 in-Hg) shall be maintained at the farthest inlet. System pressure drop shall be a maximum of 3 kPa (1 in-Hg) at the calculated demand flow rate. A flow rate of 3.3 L/s (7 scfm) per inlet shall be measured while maintaining 21kPa (6 in-Hg) at the farthest inlet.

2.9.18.3 Demand. The system demand shall be calculated based on 3.3L/s (7 scfm) per inlet-nozzle orifice. To offset piping and component losses, increase the demand flow rate by the appropriate factor from Table 9.

<u>Number of Inlets</u>	<u>Increase (%)</u>
1-20	10
21-40	15
41 and above	20

Demand Flow Rate Increase

Table 9

<u>Number of DTR's</u>	<u>Separator Tanks</u>	
	<u>Quantity</u>	<u>Minimum Size L (Gal)</u>
1- 6	1	76 (20)
7-10	1	152 (40)
11-20	1	304 (80)
21-30	2	152 (40)
31 and above	2	10.5 (2.75) per DTR

Separator Tank Sizing

Table 10

2.9.18.4 Separator Tank. The separator/collector tanks shall be sized according to Table 11. An alternative separator tank-sizing factor is 10.45 liters (2.75gallons) per DTR. The use of multiple tanks can be considered for the lower number of DTR's if continuous operation is necessary. Tank drainage piping shall slope from the tank discharge point down to the discharge point at the floor drain or standpipe receptor.

2.9.18.5 Equipment Location. The DLV equipment shall be located on or below the DTR floor level. The separator tank location shall be near the pump at the same level or directly above or below whenever feasible. When space constraints are unavoidable, after coordination with the user, or other circumstances dictate, vacuum pumps may be located above and remote from the separator tank. The pipe shall then be sized to maintain system pressure loss within the maximum limit. The tank drain valve discharge shall be a minimum

150 millimeter (0.5 foot) above the floor to accommodate the pipe slope, drain line turndown and the indirect connection air gap to the sanitary drainage system receptor. The sanitary waste centerline of pipe shall be a minimum 0.34meter (1 foot) below the floor to accommodate the floor drain trap. The equipment room shall be located as near the DTR's as possible to minimize distribution piping bends and pipe length. Equipment placement in the mechanical room shall be arranged to provide the most direct connection to the distribution piping, the sanitary waste line, and the exhaust discharge point, in that order.

2.9.18.6 Piping Distribution. The piping run from the dental utility center, located on or recessed into the floor, should continuously slope back to the vacuum source equipment with limited rise, to facilitate transportation of fluids and particulate. Minimum required slope is 0.65centimeter per 3.0 meter (1/4 inch per 10 feet). Vacuum shall be increased from the level specified in Table 8-4 at the rate of 1 in-Hg for every 1.1 foot of rise. Distribution system piping encased in the slab or buried below the slab shall be a minimum 50 millimeter (2 inch) in diameter. Where maintenance access is required, piping shall be installed in accessible locations in covered trenches, tunnels, or crawlspaces. Provide cleanout fittings at every change of direction greater than 45 degrees. Minimum access space shall be 600 millimeter (2 feet) minimum to within 600 millimeter (2 feet) of the cleanout and a minimum 150 millimeter (0.5 foot) from this point to the cleanout. Specify DWV fittings to facilitate movement of solids. Enlarging the pipe size shall be considered depending upon availability of the DWV fittings and relative pipe costs. When overhead pipe routing cannot be practicably avoided, provide cleanout fittings at the base of all risers and observe the following requirements:

- Minimize lift height by locating overhead horizontal pipe run as close to floor as possible.
- Vertical pipe run from inlet to overhead pipe shall be a minimum 40-millimeter (1½-inch) diameter.
- Overhead pipe shall be not less than 40 millimeter (1½ inch) minimum in diameter.

- The vertical pipe shall “tee” into the top of the overhead branch main.
- The available vacuum level to satisfy performance requirements stated in 8-6.18.2 shall be based on a reduction of the pump-generated vacuum at the rate of 3kPa (1 in-Hg) for each 0.33 meter (1.1 foot) rise.

2.9.18.7 Exhaust. The exhaust pipe material and size, including the connection to the equipment discharge point, shall be in accordance with manufacturer’s recommendation. The number of bends and total length shall be minimized. The exhaust piping shall be a dedicated run from the equipment connection to the discharge point outside the Medical Treatment Facility. It shall not be connected to any other piping, such as a plumbing vent line. The exhaust line shall be protected from backflow of air or liquids by detailing an appropriate discharge arrangement, such as a gooseneck or shroud with screen with a check valve, or using a flapper valve approved by the manufacturer. The discharge point shall be separated a minimum of 10 meters from the dental or medical compressed air system intakes and any HVAC system outdoor air intake(s).

2.9.19 Central Dental High-Volume Laboratory Dust Evacuation (LDE). The LDE system shall scavenge and centrally separate, filter, and collect material trimmings, grinding debris (toxic and nontoxic), and particulates from polishing and finishing operations in the dental laboratory. Point of use dust collection may be provided for some operations per using Military Department requirements.

2.9.19.1 System Components. The LDE system for dental laboratories shall consist primarily of one belt-driven vacuum pump complete with a preset, field-adjustable ingestion valve, exhaust silencer, and a central cyclonic separator with a filter bag system.

2.9.19.2 Performance. The vacuum at the farthest inlet shall be a minimum of 4.2 kPa (1.25 in-Hg). A flow rate of 28 L/s (60 scfm) per technician work station inlet and 71 L/s (150 scfm) per equipment item inlet shall be measured while maintaining the 10 kPa (3 in-Hg) at the separator. Verify the equipment requirements.

2.9.19.3 Demand. The system demand shall be calculated based on the inlet flow rate requirement. Apply the usage factor values shown in Table 11 for the given number of inlets.

<u>Lab Size (# of inlets)</u>	<u>Usage Factor (Percent)</u>	<u>Separator Filter m² (Sq. Ft.)</u>
1 to 4	100	5.6 (60)
5 to 10	80	11.2 (120)
11 to 15	70	14.9 (160)
16 to 24	60	20.5 (220)

LDE System Utilization Factors

Table 11

2.9.20 Waste Anesthesia Gas Disposal (WAGD). The WAGD system shall be a centrally piped, dry vacuum system containing two or more continuous duty pumps with a central receiver. It shall meet the requirements of NFPA 99 and be sized so that if one pump fails, the remaining pump(s) can supply 100% of the total system demand. The system design shall include automatic operation of the vacuum pumps including alternating lead/lag status. Provide an alarm to indicate vacuum pump failure that annunciates to the master medical gas alarm panel.

2.9.20.1 Applications. Disposal of waste anesthesia gas shall be incorporated into the Medical Treatment Facility design. A dedicated Waste Anesthetic Disposal (WAGD) system shall be provided in accordance with NFPA 99. When permitted by NFPA 99, the vacuum system may be used for WAGD in dental clinics. Inlets shall be provided in anesthesia locations. Verify that the system vacuum pump is suitable for the high oxygen and nitrous oxide exhaust content associated with anesthetizing procedures.

2.9.20.2 Demand and Performance. Designers shall coordinate with the Using Agency the vacuum demand level and flow requirements.

2.9.20.3 Exhaust. Vacuum shall be exhausted in accordance with NFPA 99.

2.9.21 Oxygen (OX). Oxygen (OX) is used in the gaseous state to sustain life through direct delivery to the patient. Oxygen can be stored as a gas in cylinders or as a liquid in bulk tanks. It is classified as a nonflammable gas; however it can increase the range of flammability of other materials and gases when present in sufficient concentration. Its storage requires proper construction and ventilation, in accordance NFPA 99 and NFPA 50. The oxygen system shall not be used to supply non-patient uses, including equipment in laboratories or medical equipment maintenance/repair shops. Separate point-of-use services shall be used for such non-patient applications.

2.9.21.1 Provision of Central Systems. When justified by the number of required outlets and frequency of use, central oxygen storage and distribution systems shall be provided, such as is typically the case with medical centers, hospitals, and large ambulatory care centers. Point-of-use (“roll-in”) cylinders should be utilized for clinical applications involving few oxygen outlets and infrequent utilization.

2.9.21.2 Emergency Connection. Provide an emergency oxygen supply connection on the building exterior when the oxygen supply system is located outside of the building. This connection shall be used as a temporary auxiliary source of supply. Valving and pressure control devices shall be in accordance with NFPA 99.

2.9.21.3 System Demand. The piping system shall be designed to deliver 20 L/min (0.7 cfm) at the outlet, utilizing a 100% usage factor for outlets in critical areas and the factors in Table 12 for outlets in other areas. Historical usage data from replaced or similar Medical Treatment Facilities may be used as a guideline when determining system demand instead of the method presented.

<u>Number of Outlets</u>	<u>Percent Usage</u>
1-3	100
4-12	75
13-20	50
21-40	31
41 or more	25

Oxygen System Utilization Factors

Table 12

2.9.21.4 Storage Capacity Sizing Method. In the absence of available historical oxygen consumption data, Table 13 shall be used in estimating required system storage capacity for Medical Treatment Facilities having large inpatient populations (e.g. hospitals and medical centers). For facilities with predominantly outpatient functions, designers shall work with the customer to estimate consumption rates and appropriate storage capacities.

<u>Number of Beds</u>	<u>Minimum Number of Cylinders¹</u>
1 - 50	8
51 - 75	12
76 - 100	16
101 - 125	20
126 - 150	24
Over 150	Requires special study ²

¹ Per bank of "H" cylinders

² The special study shall include an analysis of an appropriate diversity factor and the cost effective option between cylinder and bulk storage.

Cylinder Manifold Systems

Table 13

Little published data is available at present to help establish oxygen consumption on a per-outlet basis in predominantly outpatient facilities. Oxygen usage rates and procedural duration vary widely depending upon the clinical application. For example, a typical surgical procedure begins with a preparatory oxygenating period of up to 10 minutes at a consumption of 6 to 8 L/min (0.2 to 0.3 cfm). During the actual procedure, the usage rate decreases to 1 to 3 L/min (0.04 to 0.11 cfm) for a time period ranging from a fraction of an hour to several hours depending upon the nature of the surgery. A post-surgical de-nitrogenizing period of up to 10 minutes at 6 to 8 L/min (0.2 to 0.3 cfm) follows. Post-operative demands range as high as 18 L/min for recovery rooms with an average stay that ranges from 30 to 120 minutes. Oral surgery procedures usually involve a 6 L/min rate throughout the procedure. Specialty applications (e.g. pediatrics) tend to demand relatively higher usage rates. Because of these wide variations, Designers shall closely coordinate with the user to establish system demand and size satisfactory storage capacity.

2.9.21.5 Liquid Bulk-Tank Storage. Designers shall coordinate with the user to consider the economic aspects of storage capacity. Excessive capacity translates to higher utilization

costs due to boil off. Too little capacity may lead to higher costs because of more frequent tank refills, which includes vented oxygen cost as well as delivery fees. Designers shall also consider the availability of oxygen refill service. For remote locations, oversized capacity may be more practical and economical to minimize deliveries and provide for unexpected consumption increases. The selection between purchasing or leasing the bulk storage tank and ancillary equipment shall be coordinated. Both economic and logistic factors relative to the given supplier(s) shall be considered. The standard tank sizes are shown in Table 14. The tanks are normally leased with monthly rates typically ranging from \$250 to \$2000. Life cycle cost analysis will frequently show purchasing the liquid tank to be the more economical choice. In evaluating the costs associated with liquid services, be aware that the unit gas cost varies significantly with total delivery volume, presently from \$0.75 to \$1.25 per gallon for a 1895 liter (500 gallon) delivery, to as low as \$0.40 to \$0.45 per gallon for 34,065 liters (9000 gallons). Balance this consideration with boil-off costs. The average daily boil-off rate is approximately 0.5% of total tank volume.

<u>Liters</u>	<u>Gallons</u>
1,895	500
5,680	1,500
11,355	3,000
22,710	6,000
34,065	9,000
41,635	11,000
49,205	13,000
68,130	18,000
75,700	20,000

Oxygen Bulk Tank Sizes

Table 14

Fill (or purge) losses associated with the tank refill process may be significant. In tanks with a bottom-fill feature, gaseous oxygen must be purged prior to refill to lower the tank pressure below that of the delivery vessel, i.e. tanker truck. Depending upon local service availability, there are tank types and filling equipment which can minimize these losses. Top-filled tanks may be serviced without purge losses, if filling equipment is available with suitable pumps for overcoming tank pressure or utilizing the “top collapse” feature. These

should be specified when available. The top-filling procedure must be conducted only by trained personnel to avoid uncontrolled system pressure drop below minimum service levels.

2.9.21.6 System Monitoring. The central oxygen system design shall facilitate oxygen system purity monitoring with an outlet placed in the biomedical maintenance area, or other area, as directed by users. This outlet shall be upstream (on the source side) of all other oxygen outlets.

2.9.22 Nitrous Oxide (NO). Nitrous oxide is an anesthetic gas capable of inducing the first and second stages of anesthesia when inhaled. It is classified as a nonflammable gas; however, it can increase the range of flammability of other materials and gases when present in sufficient concentration. Its storage requires proper construction and ventilation in accordance with NFPA 99. Nitrous oxide manifolds shall not be located outside in cold climates due to the low vapor pressure of nitrous oxide at low temperatures.

2.9.22.1 System Demand. The piping system shall be designed to provide for a demand of 20 L/min (0.7 cfm) per outlet with the usage factors from Table 15.

<u>Number of Outlets</u>	<u>Percent Usage</u>
1-3	100
4-12	75
13-20	50
21-40	31
41 or more	25

Nitrous Oxide System Utilization Factors

Table 15

For determining storage capacity for predominantly inpatient facilities, Designers may use Table 16. For predominantly outpatient facilities, designers shall determine storage requirements from historical consumption data of similar facilities, or by consulting the user as to the probable flow rate and duration for the planned healthcare procedures.

<u>Number of Beds</u>	<u>Number of Cylinders/Bank¹</u>
50 - 100	2 expandable to 4
100 - 250	4 expandable to 6
250 - 500	6 expandable to 8
500 or More	Special Study ²

¹ Based on "G" cylinders and one complete change each week.

² The special study shall include an analysis of an appropriate diversity factor and the cost effective Option between cylinder and bulk storage.

Nitrous Oxide System Manifold Sizing

Table 16

2.9.23 Nitrogen (NI). Nitrogen is an inert gas primarily used as an operating or driving means for medical and dental hand pieces and equipment, and as an inert gas environment for laboratory uses. The cylinder manifold system shall be designed and installed in accordance with NFPA 99.

2.9.23.1 Control Cabinet. Each individual nitrogen use location (e.g., individual operating room, dental treatment rooms) shall be provided with a nitrogen control cabinet with pressure gauges and pressure regulating valves for the purpose of independently regulating pressures at that location.

2.9.23.2 Demand. The piping system shall be suitable to deliver 7 L/s (15 cfm) per outlet, with a demand usage factor of 100 percent. For the purpose of determining storage capacity, designers shall analyze the nitrogen demand of the tools and equipment intended for that facility, in consultation with the user. When this information is not available, the required storage capacity may be estimated using Table 17.

<u>Number of Using Locations</u>	<u>Cylinders per Bank *</u>
1-4	2
5-8	3
9-12	4
13-16	5
17-20	6
21-24	7
25-28	8

* Assumes "H" cylinders and one complete change each week.

Manifold Sizing for Nitrogen System

Table 17

2.9.24 Sterilization Gas. Gas/vapor sterilization may be used for treating contaminated medical equipment, implements, and certain infectious waste. In this method, the sterilizing agent is a gaseous or vaporized chemical. The two most commonly used chemicals are ethylene oxide (ETO) and formaldehyde, which may be carcinogenic.

2.9.24.1 Ethylene Oxide. All precautions in the use of ETO as outlined by OSHA (reference 8y) and NIOSH CIB 52 (reference 8z) shall be strictly followed. ETO is regarded as a potential occupational carcinogen.

- **Layout.** Where ETO is planned in a facility, a separate room for sterilizer, ETO supply cylinder, and associated piping shall be provided. Access to this equipment and storage room shall be from the Central Material Service work area only. The front of the sterilizer shall be accessed from the loading room.
- **Components.** The cylinder supply line shall have a three-way valve to permit exhausting residual ETO vapors prior to changing the tanks. The supply, tank, and vent valves shall be labeled.

- **Ventilation.** Ventilation shall also be provided for the waste gases from the sterilizer evacuation line and the drain air gap.
- **Emission Control.** Some states have adopted legislation that prohibits the release of ETO sterilizer exhaust gas to the atmosphere. Presently the only available ETO emission control technology is based on a chemical conversion or scrubber. The design shall incorporate the necessary provisions to comply with both federal and state legislation. Local requirements shall be coordinated with the user.

2.9.25 Process Gas. Process gas is natural or propane that is used as a point-of-use heat or flame source. The process is typically found in laboratories and sometimes in other areas such as equipment repair and DTR's to support medical or dental functions. The gas system design shall be in accordance with NFPA 54 and 58

2.9.25.1 Load. The load is the sum of the consumption rates for the given apparatus or equipment to be serviced. Laboratory burners are typically sized at 1465 W (5,000 Btuh) for small burners and 3075 W (10,500 Btuh) for large burners. For other equipment such as casting ovens, use manufacturer's data.

2.9.25.2 Demand is based upon the number of outlets shown in Table 18.

<u>Number of Outlets</u>	<u>Percent Usage (%)</u>
1-8	100
9-16	90
17-29	80
30-79	60
80-162	50
163-325	40
326-742	35
743-1570	30
1571-2900	25
> 2900	20

Process Gas Utilization Factors

Table 18

QUIZ

AN INTRODUCTION TO PLUMBING AND GAS SYSTEMS FOR MEDICAL FACILITIES

1. Waterborne pathogens are usually introduced into medical treatment facilities via the water supply system and _____.
 - a. sanitary drains
 - b. sinks
 - c. water closets
 - d. cooling towers

2. A domestic water temperature range of _____ is a condition that can be expected to lead to amplification of legionella bacterium.
 - a. 32 – 45 degrees F
 - b. 46 – 76 degrees F
 - c. 77 – 108 degrees F
 - d. 107 – 138 degrees F

3. To the extent economically practicable, provide a minimum of _____ water services for hospitals fed from separate mains and sources.
 - a. two
 - b. three
 - c. four, if over 50,000 SF
 - d. five, if over 200,000 SF

4. Necessary measures to prevent _____ shall be included in the design of plumbing systems for hospitals.
 - a. backflow
 - b. cross connection
 - c. back-siphonage
 - d. "a", "b" and "c"

5. All potable water discharge points, such as a faucet discharging into a reservoir, sink or tub, shall be provided with _____:
 - a. an anti-siphon valve
 - b. an adequate air gap
 - c. a check valve
 - d. an isolation valve

6. A 4-inch floor drain should not be used for design flow rates in excess of _____:

- a. 28 GPM
- b. 48 GPM
- c. 68 GPM
- d. 88 GPM

7. Common high purity water systems in medical treatment facilities may be based on _____ technology.

- a. reverse osmosis
- b. deionization
- c. ultraviolet sterilization
- d. "a", "b" or "c"

8. Treatment systems for legionella control shall be sized based on _____ water demand.

- a. total
- b. hot
- c. cold
- d. grey

9. When estimating hot water demand for a medical treatment facility, a reasonable demand to assume for each clinic sink is _____.

- a. 2 GPH
- b. 4 GPH
- c. 6 GPH
- d. 8 GPH

10. Domestic hot water for medical treatment facilities should be generated and stored at a minimum of _____ degrees F.

- a. 120
- b. 140
- c. 160
- d. 180

11. Fixtures and equipment used for sterilization and food preparation, processing or storage should be protected from contamination by _____.

- a. hydration
- b. thermal stratification
- c. osmosis
- d. backflow of waste

12. Medical gas systems include all of the following except _____.

- a. laboratory dust collection
- b. fluoridation
- c. vacuum for dental patient use
- d. waste anesthesia disposal

13. Color coding and labeling of medical gas piping shall be in accordance with _____.

- a. NFPA 7
- b. NFPA 101
- c. NFPA 99
- d. NFPA 98

14. The medical compressed air system for medical treatment facilities shall be an independent central piped system consisting of at least _____ medical compressors and a central receiver.

- a. two
- b. three
- c. four
- d. (there is no recommendation)

15. Air drying systems shall include an air dryer of either the mechanical refrigeration or _____ type.

- a. thermal exchange
- b. dessicant
- c. entropic
- d. enthalpic

16. Dental compressed air (DCA) shall be provided by _____ or more compressors.

- a. one
- b. two
- c. three
- d. four

17. A dental laboratory with 10 outlets for compressed laboratory air (LA) would require a laboratory air system capable of delivering at least _____ CFM of compressed air.

- a. ten
- b. seven
- c. five
- d. three

18. An instrument air (IA) system is intended to be used to power medical devices not related to _____ .

- a. flammable liquids
- b. human respiration
- c. surgical procedures
- d. blood test procedures

19. The system vacuum operating range for a dental low vacuum (DLV) shall be _____ in-Hg.

- a. 3 to 4
- b. 4 to 6
- c. 6 to 8
- d. 8 to 10

20. The minimum vacuum in the receiver of a dental high vacuum (DHV) system shall be _____ in-Hg.

- a. 16
- b. 17
- c. 18
- d. 19

21. When calculating hot water demand for a medical treatment facility domestic hot water system, a reasonable assumption for a single leg whirlpool bath is _____ gallons per hour.

- a. 5
- b. 10
- c. 100
- d. 20

22. In kitchen areas in medical treatment facilities, the domestic hot water supplied to dish and pot washing equipment should be a minimum of _____ degrees F.

- a. 150
- b. 160
- c. 170
- d. 180

23. For a dental clinic which includes a dental laboratory, which of the following is not one of the compressed air/vacuum systems not normally required?

- a. process air
- b. compressed air
- c. low volume oral evacuation vacuum
- d. high volume oral evacuation vacuum

24. When a mechanical refrigeration system is to be used for air drying in a medical treatment facility compressed air system the equipment shall have a cycling feature on all compressors under _____ HP to minimize the possibility of icing and moisture carry-over.

- a. 3
- b. 5
- c. 7
- d. 10

25. For an instrument air system (IA), at least _____ compressors, or one with a standby header must be provided as a minimum.

- a. 2
- b. 3
- c. 4
- d. (no minimum number)